

# Improving the dry magnetic separation of BOF-slag by applying an innovative pre-treatment process



Iron recovery, Slow-Cooling, Crystallite Structure, Microwave-Treatment, Intergranular Cracks, Grinding

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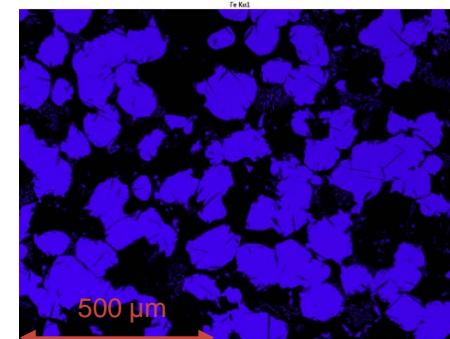


Stahl

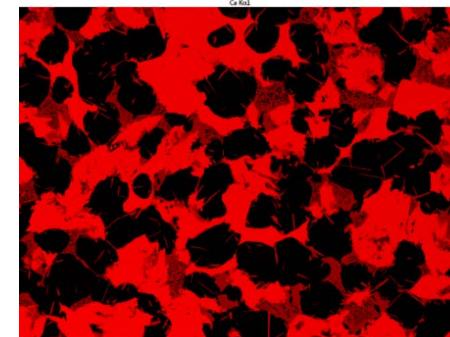
# Motivation and Process Concept

- › Motivation:
  - › 8 Mt of BOF-slag produced in EU in 2018\*
  - › Only 15.3% of BOF-slag recycled internally\* → **limitation due to P-content**
  - › Fe-content ~ 20%
  - › Move towards a circular economy
- RFCS Project SLAGREUS

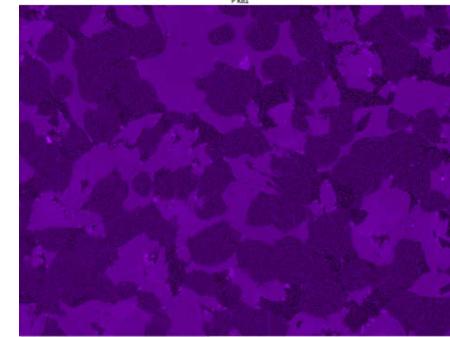
- › Process Concept:
  - › Separation into Fe-rich/P-poor fraction and a Ca-/P-rich fraction
  - › Fe-rich (Oxides, Ferrites) → fine ore substitute in sinter plant
  - › Ca-/P-rich → external use as reactive cement additive, raw meal additive or fertilizer



Fluorescence: Fe K $\alpha$ 1



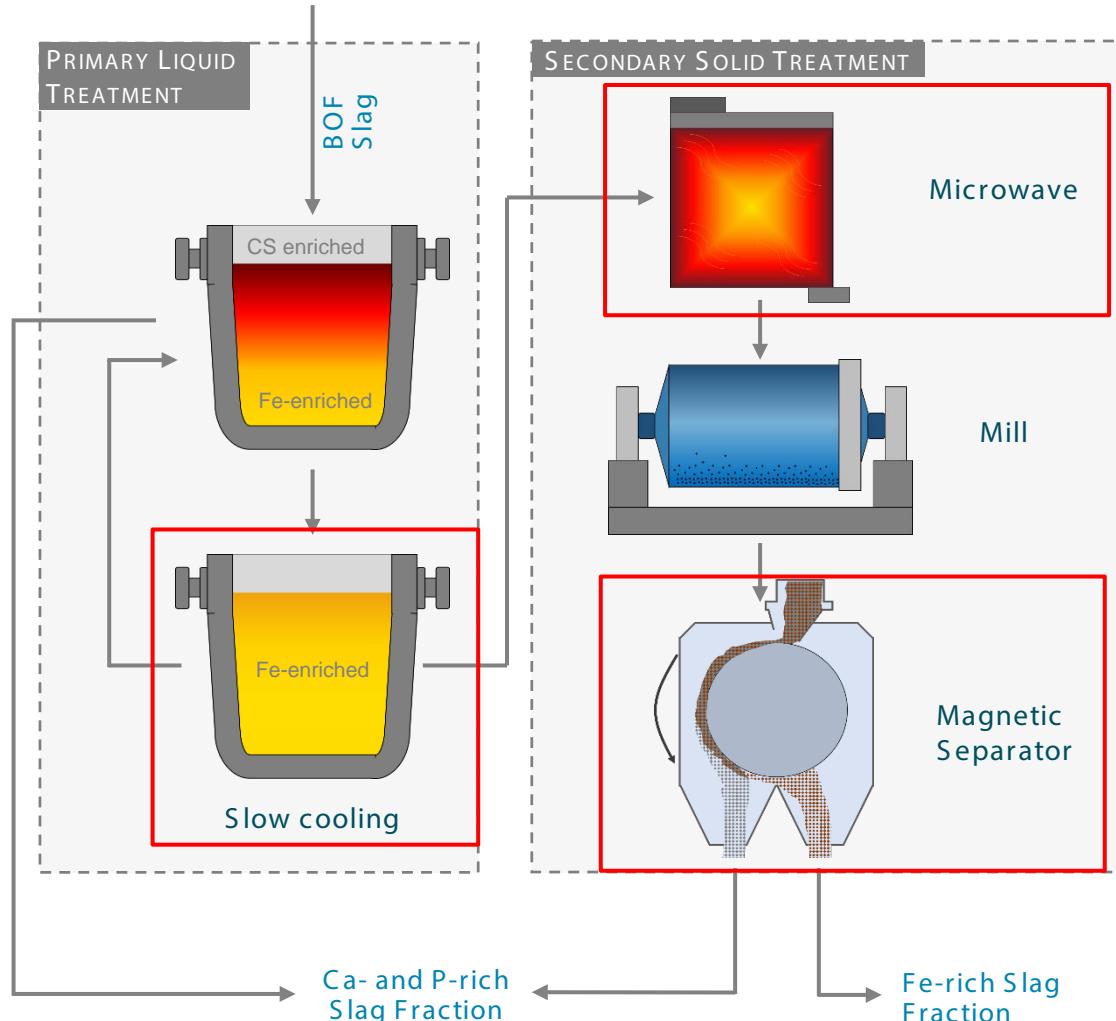
Ca K $\alpha$ 1



P K $\alpha$ 1

\*<https://www.euroslag.com/products/statistics/statistics-2018/>

# SLAGREUS Process Concept



SLAGREUS BOF-slag recycling process concept

1. Primary Liquid Treatment:
  1. Segregation of Ca/P-rich fraction in liquid state → reduce need for secondary treatment
  2. Slow cooling of remaining Fe-rich fraction → large crystal grains facilitate secondary treatment
2. Secondary Solid Treatment of Fe-rich fraction
  1. Microwave pre-treatment → intergranular cracks
  2. Grinding → liberate mineral phases
  3. Magnetic separation → obtain +Fe/-P fraction and +Ca/+P fraction

# Primary Liquid Treatment

## Slag Yard Compartment Test:



Slag Mixing



O<sub>2</sub>-Injection + Slow Cooling

## Slag Pot Test:



Slag Mixing



O<sub>2</sub>-Injection



Slow Cooling

Self insulating  
properties for slow  
cooling

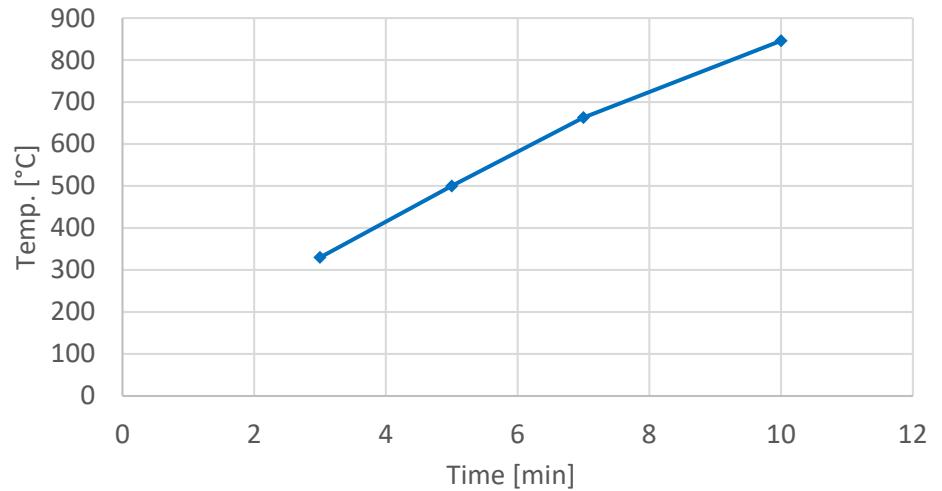


Enlarged crystal  
grain size

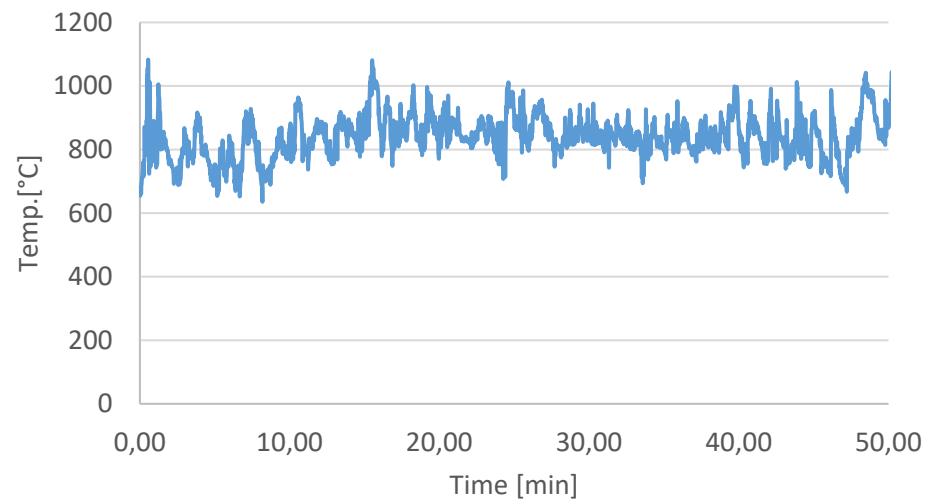


	Reference standard BOF slag	Overblown in converter + slow cooling	Liquid oxidation + slow cooling in slag yard	Liquid oxidation + slow cooling in slag pot
Q3(100µm) [wt.%]	100.0	17.5	53.8	57.1
Fe-content [wt.%]	24.4	40.5	23.8	20.1

## Microwave Treatment – Setup



Batch operation: Multimode 4 kW 2.45 GHz. Max. batch size: 1.2 kg



Continuous operation: Resonance cavity max. 30 kW 915 MHz. Throughput: 5 – 10 kg/h\*

\*<https://ceinnmat.com/>

# Microwave Treatment – Effect

## Dysfunctional Parameters

Ionisation

Arcs + plasma

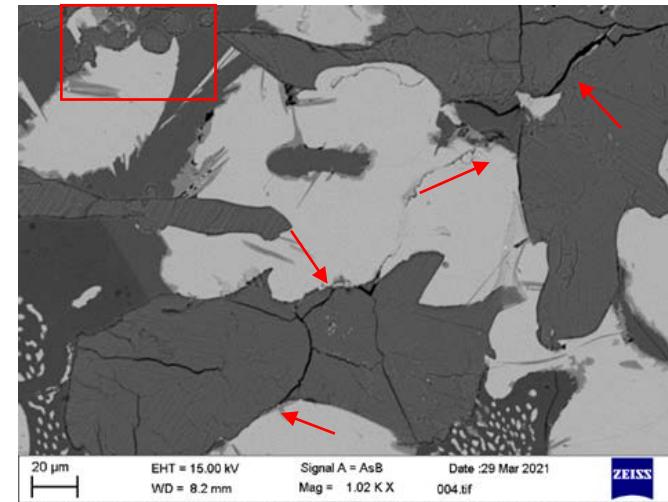


Surface melting

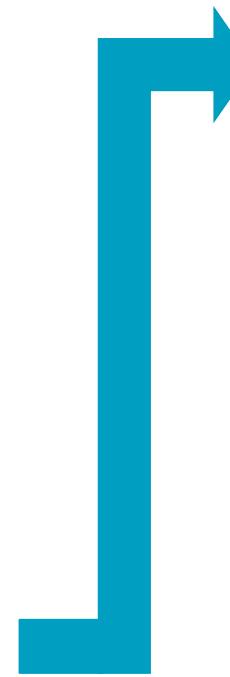
## Adapted Parameters

Rapid heating of Fe-phases

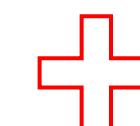
Thermal shock



Intergranular crack formation

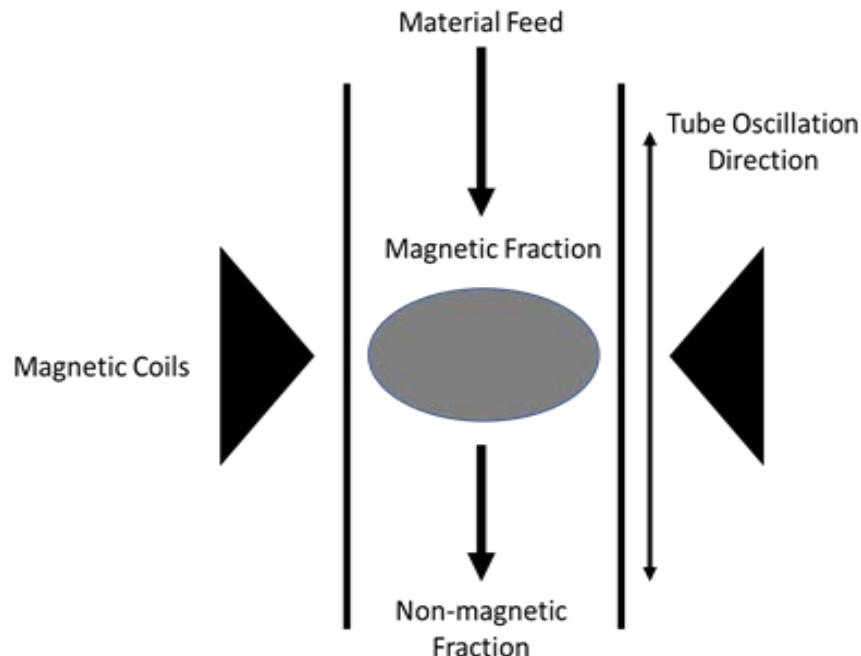


	Untreated	Irradiated 4 kW 10 min
Grindability Wi [kWh/t]	23.4	19.9
Liberation [%] (mass fraction of particles $\text{FeO}_x \geq 80\%$ )	20.2	36.4
Magnetisation [%] (SATMAGAN)	0.4	2.0

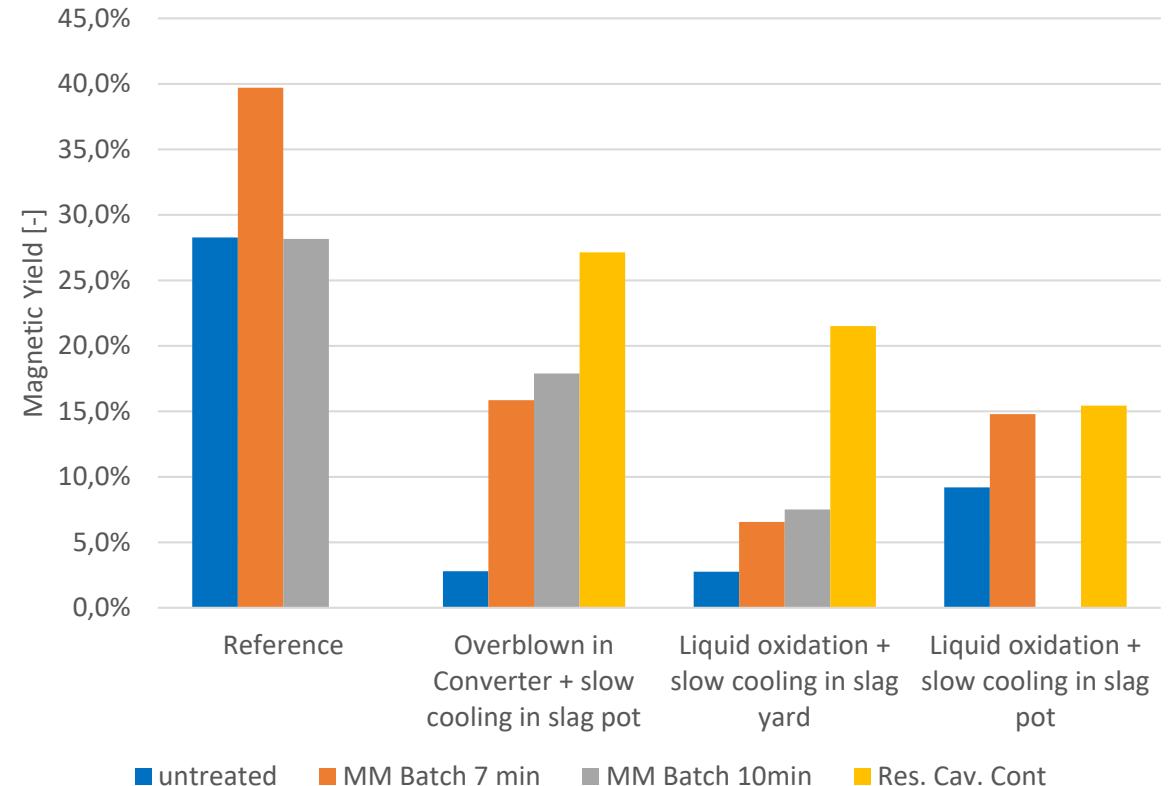


Solid-State Oxidation

# Dry Magnetic Separation (Lab Scale)



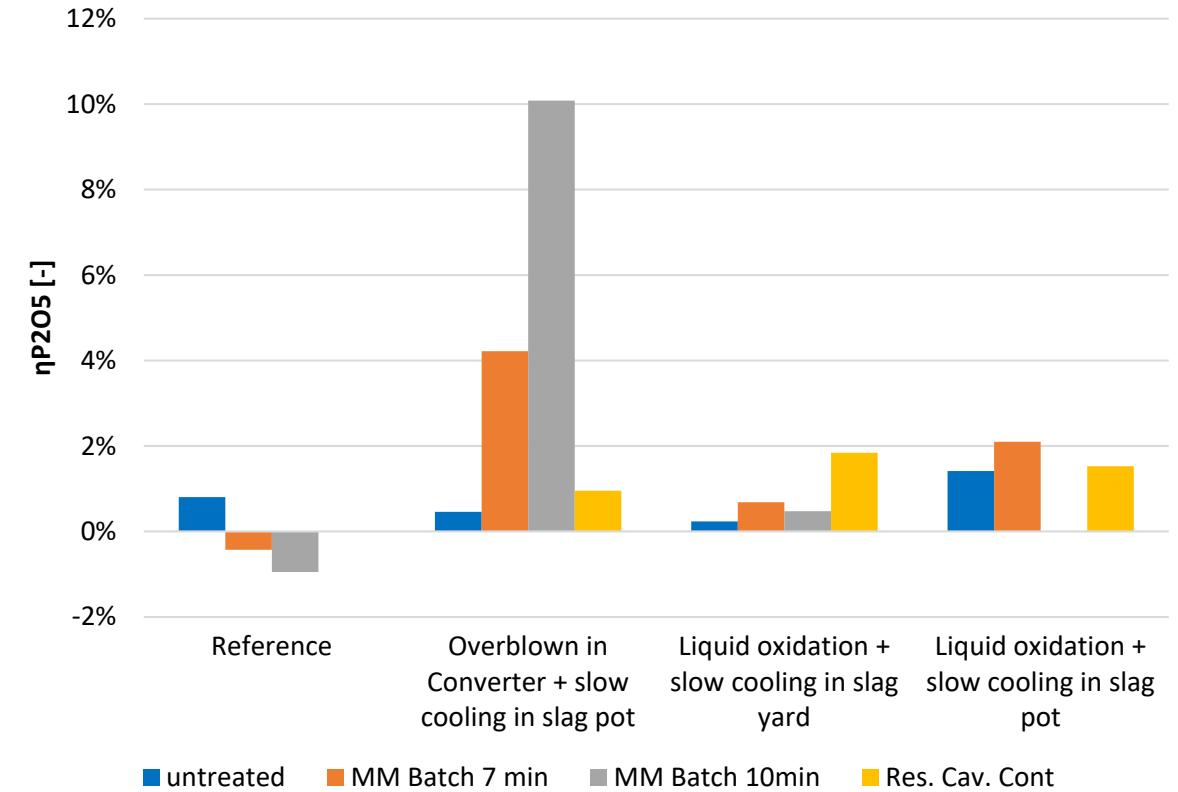
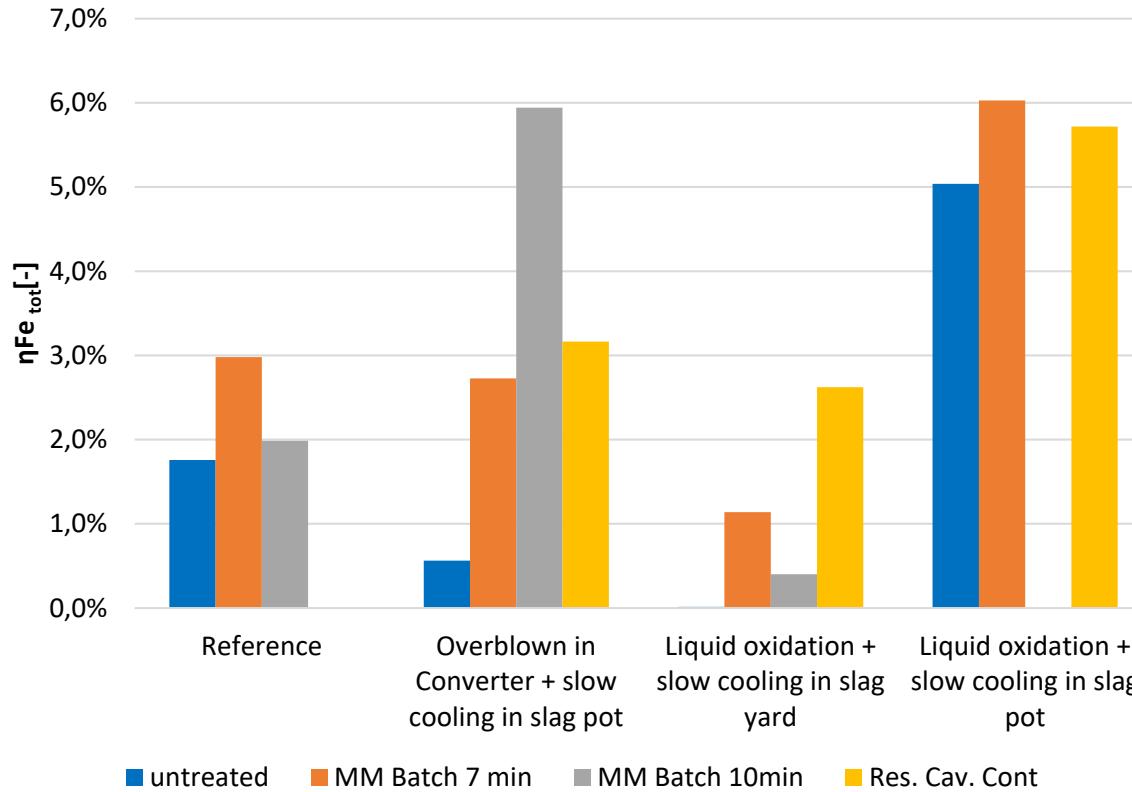
Davis tube (max 1.4 T) used for dry magnetic separation.



Agglomeration → Feed particle size range 56 µm to 100 µm

Increase in microwave irradiation duration/ intensity  
→ Increase in magnetic yield of the dry magnetic separation (DMS)

# Dry Magnetic Separation (Lab Scale)



Overall evaluation of separation → Separation degree  $\eta$  adapted from Luyken and Bierbrauer

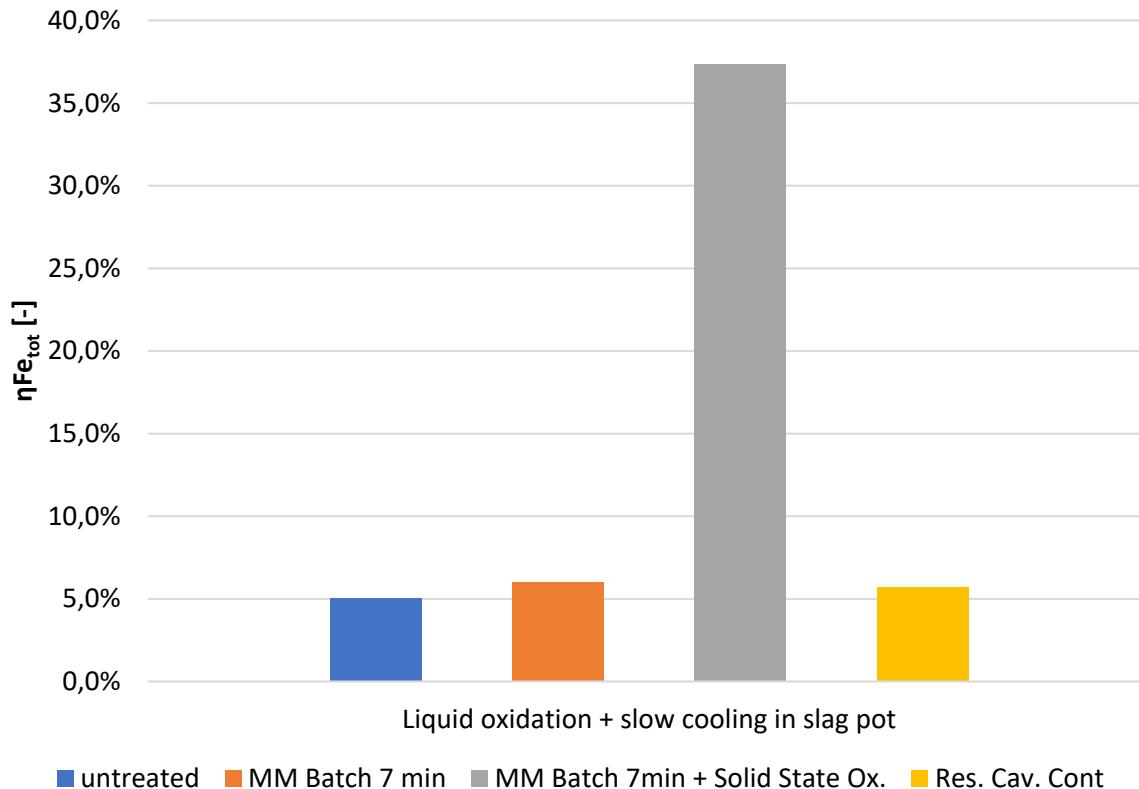
$$\eta_i = \text{Recovery of resource} - \text{Recovery of byproduct}$$

Microwave irradiation → overall positive effect on  $\eta$

# Effect of Solid-State Oxidation on DMS

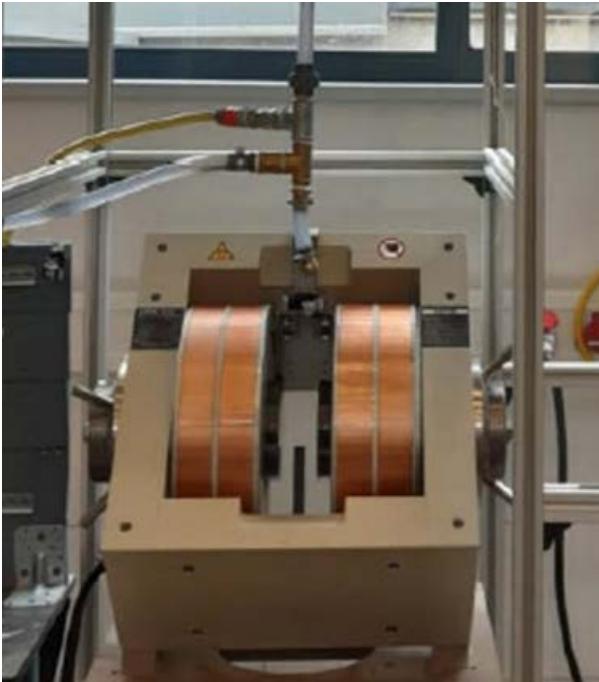
## Sample Preparation:

1. Grinding
2. Separation of 56-100 $\mu$ m fraction
3. Annealing for 1h at 900°C under ambient air



- Magnetic separation with variable settings now possible → optimisation
- Increase of  $\eta_{Fe}$  by factor 6
- Increase of  $\eta_{P2O5}$  from 2.1% to 11.1%

# Dry Magnetic Separation (Pilot Scale)



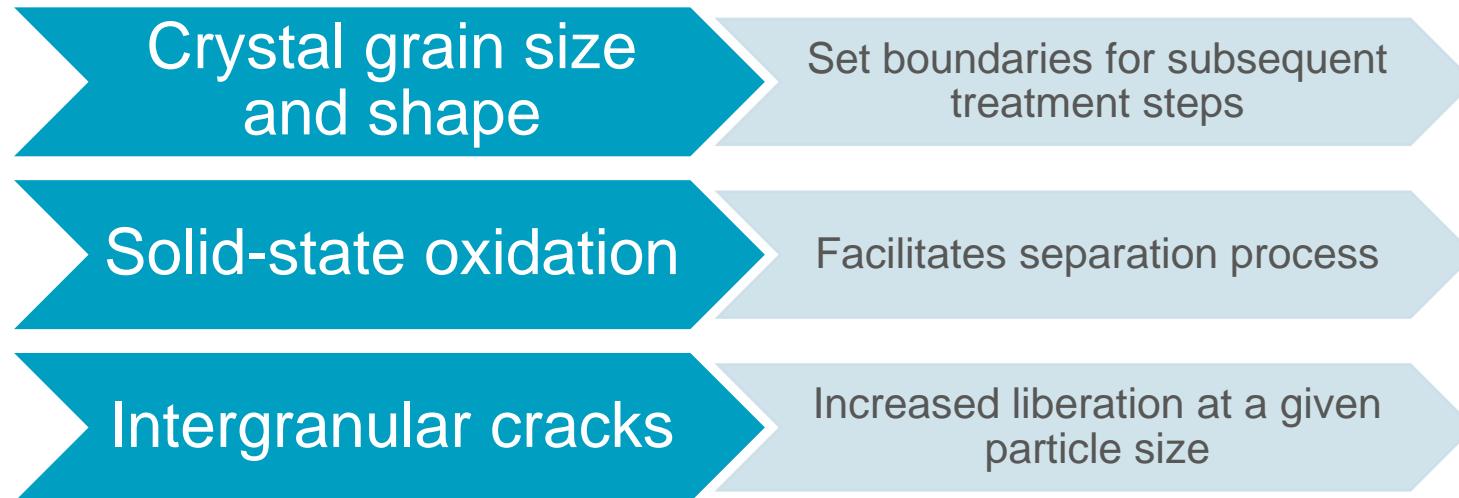
Air Stream Matrix Separator\*



Low Intensity Magnetic Drum Separator (LIMS)\*

$\eta_{Fe}$ [%]	Davis Tube	Air Stream Matrix Separator	LIMS
<b>Liquid oxidation and slow cooled in slag yard Irradiated in Resonance Cavity</b>	2.62	7.33	0.25
<b>Slow cooling in slag pot Oxidized</b>	37.34	11.72	12.60

\*Montanuniversität Leoben Lehrstuhl für Aufbereitung und Veredelung



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**Outlook:** Can solid state oxidation be done using waste heat?

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Is it possible to tune high power microwave treatment to achieve homogenous thermal shock?

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Can the produced slag fractions be utilised in the sinter plant (Fe-rich) and cement/fertilizer production (Ca-rich)?



Research Fund  
for Coal & Steel



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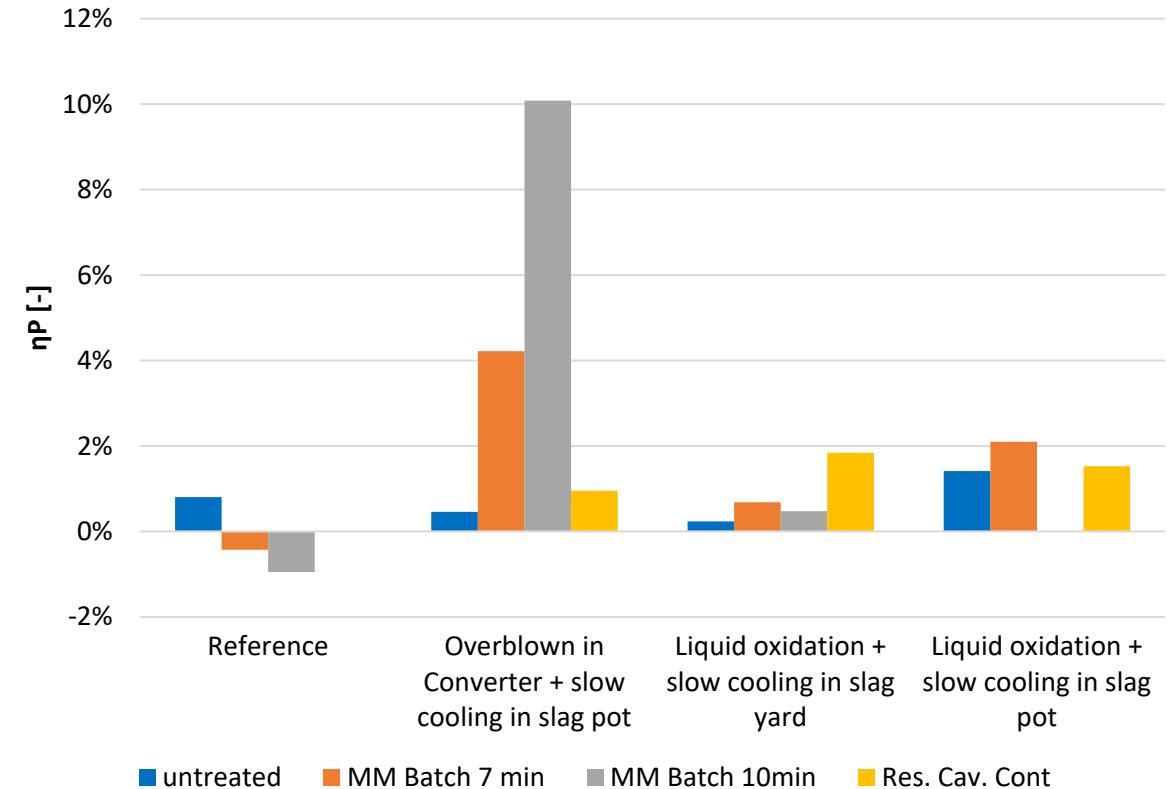
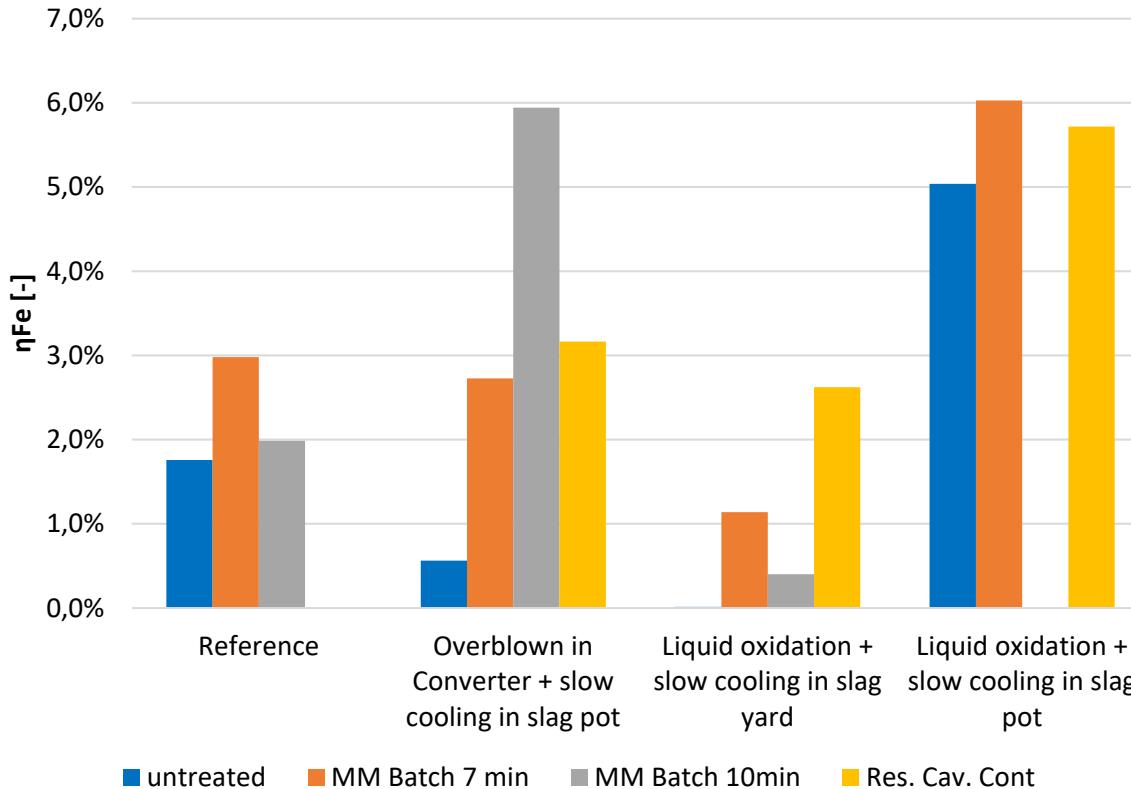
ONE STEP AHEAD.



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# Dry Magnetic Separation (Lab Scale)



Overall evaluation of separation → Separation degree  $\eta$  adapted from Luyken and Bierbrauer

$$\eta_i = \frac{(w_{i,Magnetic} - w_{i,Feed}) \cdot (w_{i,Feed} - w_{i,NonMag})}{w_{i,Feed} \cdot (1 - w_{i,Feed}) \cdot (w_{i,Magnetic} - w_{i,NonMag})}$$

Reference → untreated

	CaO (%)	Fe (%)	P2O5 (%)	w [-]
Feed	38,39	24,92	1,01	
Conc.	37,45	26,09	0,98	0,28
Tailings	38,76	24,47	1,02	0,72

Slag Pot → untreated

	CaO (%)	Fe (%)	P2O5 (%)	w [-]
Feed	40,64	19,22	1,05	
Conc.	35,69	27,72	0,89	0,09
Tailings	41,14	18,36	1,07	0,91

Slag Pot → MM

	CaO (%)	Fe (%)	P2O5 (%)	w [-]
Feed	41,65	20,00	1,10	
Conc.	36,914	26,514	0,944	0,15
Tailings	42,473	18,864	1,125	0,85

Slag Pot → MM → Ox

	CaO (%)	Fe (%)	P2O5 (%)	w [-]
Feed	40,37	22,58	1,04	
Conc.	31,39	34,45	0,83	0,55
Tailings	51,33	8,08	1,30	0,45